

# **Technical Notes**

# Comparison of Two Types of Combined Measures, STI and $U_{50}$ , for Predicting Speech Intelligibility in Classrooms

## Young-Ji CHOI

Department of Architectural Engineering, Kangwon National University 1 Kangwondaehak-gil, Choncheon-si, Kangwon-do, 200-701, Korea; e-mail: youngjichoi@kangwon.ac.kr

(received November 9, 2016; accepted April 28, 2017)

The present study reports on the speech intelligibility as measured by speech transmission index (STI) and useful-to-detrimental sound ratios  $(U_{50})$  in university classrooms. Acoustic measurements were made in 12 quietly occupied university classrooms. The measured impulse responses of the classrooms were used to determine the modulation transfer function, m(F), for the STI calculation according to IEC 60268-16.  $U_{50}$  values were determined from both signal-to-noise ratios (SNR) and  $C_{50}$  values. The mean STI and frequency-weighted  $U_{50}$  values for the 12 occupied classrooms were strongly linearly related. The results showed that classrooms with  $U_{50}$  values of about +0.5 dB correspond to STI values of 0.60, indicating 'good' acoustical conditions for speech intelligibility. The results illustrate that the  $U_{50}$  measure can be a more practically useful means of assessing and understanding room acoustics conditions for real speech communication in active classrooms.

**Keywords:** speech intelligibility; speech transmission index; useful-to-detrimental sound ratios; classrooms.

**PACS no.** 43.55 Br, 43.55 Ev.

#### 1. Introduction

Two combined measures, speech transmission index (IEC 60268-16, 2011) and useful-to-detrimental sound ratios (BRADLEY et al., 1999) can be considered complete predictors of speech intelligibility in classrooms because they include both a measure of room acoustics quality and a measure of speech-to-noise-ratios. Previous studies (BRADLEY et al., 1999; BRADLEY, YANG, 2009) have shown that room acoustics and signal-tonoise-ratios (SNR) both influence speech intelligibility in classrooms and hence the combined effect of room acoustics and SNR on speech intelligibility should be measured. The ratio of early-arriving to late-arriving sound  $(C_{50})$  has been used as a measure of the effects of room acoustics on the clarity of speech sounds in classrooms (BRADLEY, 1986), but this measure cannot estimate the combined effects of room acoustics and background noise.

Useful-to-detrimental sound ratios  $(U_{50})$  are defined as the logarithmic ratio of the useful to the detrimental sound (BRADLEY *et al.*, 1999). The useful sound is the early-arriving speech energy and the detrimental sound is the sum of the later-arriving speech energy and the ambient noise energy. Useful-

to-detrimental sound ratio values  $(U_{50})$  can be determined from both signal-to-noise ratios and  $C_{50}$  values; see Eq. (1) (BRADLEY *et al.*, 1999). The  $U_{50}$  measure can explain the combined effects of room acoustics and SNR values on the resulting speech intelligibility. It attempts to correctly include the balance of the importance of the SNR and acoustic clarity of the room.

$$U_{50} = 10 \log \left\{ \frac{E/L_{50}}{1 + (E/L_{50} + 1)N/S} \right\}, \quad \text{dB}, \qquad (1)$$

where N is the ambient noise energy, S is the speech energy, and  $E/L_{50}$  is the linear early-to-late arriving sound energy ratio.

The  $U_{50}$  measure combines the detrimental effects of late arriving speech and ambient noise relative to the useful direct and early reflected speech sounds and thus being able to achieve the best combination of maximising both clarity ( $C_{50}$ ) and G values for optimum conditions in classrooms.

Classroom quality was strongly correlated with the background noise level and the related signal-to-noise ratios (HODGSON, 2002), emphasising the need for the design criteria for occupied classrooms (HODGSON, NOSAL, 2002). A number of studies (HODGSON *et al.*, 1999; SATO, BRADLEY, 2008) have reported that the speech and noise levels are quite different from values measured in active classrooms with the influence of noise due to students' activity. They also proposed a method for estimating SNR values in classrooms when they are occupied and in operation. The results of the active classroom acoustics studies (HODGSON *et al.*, 1999; SATO, BRADLEY, 2008) indicate greater noise levels than recommended in the ANSI standard for classroom acoustics (ANSI S12.60, 2004).

Among three types of combined measures  $(U_{50},$  $AL_{\rm cons}$ , STI) for speech intelligibility,  $U_{50}$  was the most accurate predictor and explained 97% of the variance in speech intelligibility scores (BRADLEY et al., 1999). Because the  $U_{50}$  measure is based on the same basic concepts and can be calculated from commonly measured parameters (e.g.,  $C_{50}$  and SNR values), it can be a more practically useful means of assessing and understanding room acoustics conditions for speech. This is the main reason for further exploring the merits of using  $U_{50}$  in this study. However, for  $U_{50}$  there is no standard procedure for combining information at different frequencies or for the relative importance of signal-tonoise and room acoustics components. BRADLEY et al. (1999) found that both A-weighted and AI frequencyweighted sums of the octave band  $U_{50}$  values were well correlated with speech intelligibility scores. Thus these frequency-weighted measures are generally acceptable as broadband measures because they do include effects in all frequency bands of interest. In a recent study (BRADLEY, 2011),  $U_{50}$  values were calculated by combining octave band values following the procedure used in calculating AI and STI values and using the frequency weightings from the STI measure.

NIJS and RYCHTÁRIKOVÁ (2011) proposed a conversion from measured STI values to quality classification applied to  $U_{50}$  values. That is, classifications of STI in 0.15 steps 'bad' to 'excellent' were used for  $U_{50}$  in 5 dB steps. But they did not use the frequency weightings from the STI measure (IEC 60268-16, 2011) for calculating  $U_{50}$  values. BRADLEY and BISTAFA (2002) proposed a better indication of the general relationship between 1-kHz  $U_{50}$  values and mean speech intelligibility scores using a new regression equation. They showed that a 1-kHz  $U_{50}$  value of +2 dB is a reasonable goal for conditions that would permit very good speech communication in rooms. A 1-kHz  $U_{50}$ value of +2 dB proposed by BRADLEY and BISTAFA (2002) acoustical conditions for speech intelligibility given in NIJS and RYCHTÁRIKOVÁ'S (2011) classification. The results reported in previous studies (NIJS, RYCHTÁRIKOVÁ, 2011; BRADLEY, BISTAFA, 2002) demonstrate that both measures are highly correlated and essentially describe the same properties of the rooms.

This paper is a follow-up of a previous work (CHOI, 2016) that experimentally investigated the effect of occupancy on acoustical conditions in university classrooms. The present study reports on the speech intelligibility as measured by speech transmission index (STI) and useful-to-detrimental sound ratios  $(U_{50})$  in university classrooms. Acoustical measurements were made in 12 quietly occupied university classrooms. The measured impulse responses of the classrooms were used to determine the modulation transfer function, m(F), for the STI calculation according to IEC 60268-16 (2011).  $U_{50}$  values were determined from both signal-to-noise ratios (SNR) and  $C_{50}$  values. The goal of the present work is to further explore the merits of using  $U_{50}$  to measure the combined effects of room acoustics  $(C_{50})$  and SNR values on speech intelligibility in classrooms essentially as accurately as STI values. It is hoped that one can use a linear regression to convert values of one measure to values of the other measure.

#### 2. Measurement procedures

### 2.1. Measurements of room acoustical qualities in classrooms

Table 1 presents the data describing the 12 university classrooms used for the measurements in a previous paper (CHOI, 2016). Of the 12 classrooms, 9 were typical classrooms, and 3 were used for computers, teleconferences, and conferences. Seven classrooms had rectangular shapes with windows on one side and 5 classrooms had non-rectangular shapes. The mean percentage of seats occupied during the measurements was 54%. Speech-reinforcement systems were installed in some larger sized classrooms, but they were not in operation during the measurements. The occupants were allowed to choose where they wished to sit. In the occupied classroom measurements, the students were asked to remain quiet. Thus, the noise measurements did not include significant student activity.

The classrooms varied from small lecture rooms with volumes about 190 m<sup>3</sup>, to a large conference hall with a volume of about  $2500 \text{ m}^3$ . Six classrooms had similar room finishes with reflective surface materials such as: painted concrete walls, terrazzo floors, and were mostly used for small to medium size classes with fewer than 100 occupants. The other 6 classrooms had mostly porous absorbing surface materials. Four of these 6 classrooms were lecture theatres for larger sized classes including up to 240 occupants. The mean midfrequency  $T_{30}$  (500–1000) values for the six occupied and unoccupied reflective classrooms were 0.81 s and 1.32 s. The other 6 classrooms had mostly porous absorbing surface materials and vinyl or fabric covered chairs. Four of these 6 classrooms were lecture theatres for larger sized classes including up to 240 occupants. The mean mid-frequency  $T_{30}$  (500–1000) values for the six occupied and unoccupied absorptive classrooms were 0.53 s and 0.60 s. More details of the 12 classrooms are included in Ref. 7.

Rooms	Width	Depth	Height	Volume	Number	Mean $T_{30}$ unoccupied	Mean $T_{30}$ occupied
	[m]	[m]	[m]	$[m^3]$	of occupants	[8]	$[\mathbf{s}]$
#1	9.0	7.1	3.1	199	15	1.29	0.89
#2	9.1	7.2	2.9	193	11	0.83	0.72
#3	8.9	10.6	3.0	284	22	1.18	0.82
#4	8.8	10.1	2.8	248	13	1.15	0.84
#5	7.9	16.6	2.7	354	62	1.81	0.83
#6	7.4	11.9	2.7	238	46	1.68	0.77
#7	17.5	17.2	4.4	1310	84	0.56	0.55
#8	13.9	15.8	5.6	1227	80	0.74	0.57
#9	17.0	16.2	2.5	690	61	0.44	0.39
#10	6.4	13.1	2.7	226	48	0.31	0.26
#11	16.5	21.1	7.3	2535	53	0.92	0.84
#12	17.5	15.9	3.2	888	74	0.65	0.58
Mean	11.7	13.6	3.6	699	47	0.96	0.67
s.d.	4.4	4.3	1.5	707	27	0.47	0.20
Max	17.5	21.1	7.3	2535	84	1.81	0.89
Min	6.4	7.1	2.5	193	11	0.31	0.26

Table 1. Data for 12 university classrooms used for the measurements including mean (500–1000 Hz)  $T_{30}$  values for both occupied and unoccupied cases.

Room acoustical quantities were determined from the measured impulse responses in occupied classrooms. A logarithmic sine sweep signal was used as the source signal and was radiated into the classroom from a dodecahedron loudspeaker (Norsonic, Nor276). Measurements were made at six to nine receiver positions using 1/2'' free-field microphones (G.R.A.S, Type 46AF) evenly distributed among the seated occupants in each classroom, at a height of 1.2 m. One centre source position at a height of 1.5 m was used.

The reverberation times  $(T_{30})$ , the early-to-lateenergy ratios  $(C_{50})$ , and the strength (G) were measured in accordance with ISO 3382 (2003) using the Dirac software V.6.0 (Brüel & Kjær, 2014). The actual ambient noise levels were measured at each receiver position in each classroom. Useful-to-detrimental sound ratios were calculated using Eq. (1). The octave band energy ratios were weighted with the same frequency weightings as used in the STI measure (IEC 60268-16, 2011) before summing to give the overall  $U_{50}$  values.

# 2.2. Calculation of expected speech levels at each receiver position

An ideal talker was assumed, to be located at the position of the sound source and speaking with a 'raised voice level' according to that specified in ANSI S3.5 (1997). The expected speech levels at each receiver position were calculated assuming the source level at 1 m from the source was the ANSI 'raised voice level' and corresponding source spectrum. The expected attenuation to each receiver position was calculated from the measured G values using the following Eq. (2)

Atten = 
$$L_{\rm ss} - L_{\rm rs} = -G + 20$$
, dB, (2)

where attenuation is a positive value representing the reduction in level from a distance of 1 m to a distance of r m from the speech source.  $L_{\rm ss}$  is the direct speech sound level, 1 m from the source, and  $L_{\rm rs}$  is the speech sound level at the receiver position.

The measured G values can be used to determine the attenuation of sound from the source position to that expected at each receiver position simply by correcting G values to be relative to a reference level at 1 m rather than 10 m. They should precisely predict the effect of the measured sound attenuation on the source levels and therefore give the correct expected speech levels at each receiver position using the following Eq. (3):

$$L_{\rm rs} = L_{\rm ss} - \text{Atten} = L_{\rm ss} + G - 20, \quad \text{dB.}$$
 (3)

#### 2.3. Calculation of speech transmission index

The measured impulse responses of the classrooms were also used to determine the modulation transfer function, m(F), for the STI calculation according to IEC 60268-16 (2011). The modulation transfer function at modulation frequency F, (m(F)), can be calculated from room impulse responses and the effective signal-to-noise ratio, S/N (in dB), using the following Eq. (4) (SCHROEDER, 1982):

$$m(F) = \frac{\left| \int_{0}^{\infty} h^{2}(t) e^{-2\pi F t} \, \mathrm{d}t \right|}{\int_{0}^{\infty} h^{2}(t) \, \mathrm{d}t} \cdot \frac{1}{1 + 10^{\frac{-S/N}{10}}}, \quad (4)$$

where F is a modulation frequency, h(t) is an impulse response, and S/N is the speech signal-to-noise ratio in dB. The STI value is calculated from a weighted average of modulation transfer index (MTI). The IEC 60268-16 (2011) describes this calculation and also considers masking effects and the absolute threshold of masking for the calculation of the revised speech transmission index.

#### 3. Results and discussion

# 3.1. The combined effect of room acoustics and background noise

It is well known that good acoustical design for speech communication requires one to maximise the signal-to-noise ratio and provide optimum room acoustics conditions in classrooms This process is to find an optimum reverberation time that maximises the 'useful' components (the combination of the direct and early-reflected sound) of the speech sounds relative to the 'detrimental' (the sum of the late-arriving speech sounds plus the ambient noise) components. For example, in very quiet conditions the ambient noise levels will be much lower than the late-arriving speech sound energy and hence the amount of late-arriving energy will predominate for the detrimental components. For such conditions varying the reverberation time will have large effect on achieving optimum room acoustics conditions in classrooms.

In this study,  $U_{50}$  values were calculated by averaging octave band values from 125 to 4000 Hz and using the frequency weightings from the STI measure following the procedure used in BRADLEY'S study (2011). Using a non-frequency weighted calculation of  $U_{50}$  values is not appropriate because this would overemphasise the importance of the low frequencies when the intention is to predict expected speech intelligibility. Table 2 compares the results of linear regression fits of various broadband useful-to-detrimental sound ratio measures to STI values. For example,  $U_{50}$  (A, 125– 4000) indicates  $U_{50}$  values obtained from A-weightings of the octave band  $C_{50}$  and speech and noise levels and averages of the octave band values from 125 to

Table 2. Results of linear regression fits of various broadband useful-to-detrimental sound ratio measures to STI values.

Measure	$R^2$
$U_{50}$ (125–4000)	0.961
$U_{50}$ (500–4000)	0.952
$U_{50}$ (A, 125–4000)	0.948
$U_{50}$ (A, 500–4000)	0.952
$U_{50}$ (STI, 125–4000)	0.968
$U_{50}$ (STI, 500–4000)	0.953

4000 Hz. The  $U_{50}$  (STI, 125–4000) values, obtained from STI-weighted averages of the octave band values from 125 to 4000 Hz, were best correlated with the STI values and led to an  $R^2$  value of 0.968 shown in Table 2. They showed a slightly better correlation than the  $U_{50}$  (STI, 500–4000) values averaging over the four octave bands from 500 to 4000 Hz ( $R^2$  value of 0.953). The frequency-weighted  $U_{50}$  values seem to be more reliable as a broadband measure because they appear in all frequency bands of interest.

Figure 1 plots the calculated mean, frequencyweighted,  $U_{50}$  (STI, 125-4000) values versus the measured mean  $C_{50}$  values for the 12 occupied classrooms. The mean overall  $U_{50}$  and  $C_{50}$  values for the 12 occupied classrooms in Fig. 1 show a good fit to the linear regression line with a small amount of scatter  $(R^2 = 0.944$  and the standard deviation about the regression line,  $\sigma = 0.015$ ). Only two classrooms deviate much from the linear regression line. These were classrooms #1 and #8 where measurements included air conditioner noise. The increased noise for these rooms leads to lower  $U_{50}$  values for similar  $C_{50}$  (125–4000) values. For example the results for classroom #8 deviate 9.8 dBA below the regression line indicating lower SNR values than for the main trend. The results in Fig. 1 indicate that  $U_{50}$  values are mostly related to the corresponding  $C_{50}$  values except for rooms #1 and #8 where the increased ambient noise levels further reduce the  $U_{50}$  values. A  $C_{50}$  value of +1 dB or greater has been suggested (BRADLEY, 1986) to be required for good conditions for speech communication, which corresponds a frequency-weighted  $U_{50}$  value of +0.11 dB or greater from the regression line in Fig. 1.



Fig. 1. Calculated mean frequency-weighted  $U_{50}$  (STI, 125–4000) values versus measured mean  $C_{50}$  values averaged of the octave bands 125 Hz to 4000 Hz for the 12 occupied classrooms.

The frequency-averaged  $C_{50}$  and  $U_{50}$  results show the more general trends of how the SNR values would affect the intelligibility of speech sounds in the groups of classrooms. The 6 more absorptive classrooms (symbols for filled circles) having decreased later arriving reflection energy lead to increased  $C_{50}$  values by about 4.3 dB relative to the results for the 6 more reflective classrooms (symbols for empty circles). However, shorter reverberation times led to larger reductions in speech levels and hence decreased SNR values. This resulted in a larger reduction in  $U_{50}$  values for the more absorptive classrooms in Fig. 1. Overall the  $U_{50}$  values indicate that the negative effect of reduced speech levels was greater than the positive effect of increased clarity.

# 3.2. Comparison of predictors of speech intelligibility

The results for both measures are compared in Fig. 2 which is a plot of STI values versus  $U_{50}$  (STI, 125–4000) values. The measured SNR values were included in the calculation of both STI and  $U_{50}$  values. The data in Fig. 2 show that the 6 more reflective classrooms (symbols for empty circles) have lower STI values even if the SNR values are more than 15 dBA. That is, the effects of room acoustics are more predominant than the SNR values in these reflective classrooms  $(T_{30} (500-1000) > 0.7 \text{ s})$ . For such conditions, the amount of late-arriving energy will predominate for the detrimental components and hence decrease speech intelligibility. However, the results for two absorptive classrooms  $(T_{30} (500-1000) < 0.7 \text{ s})$  show that the SNR component is more critical for obtaining close to optimum conditions for speech. If the classrooms have more ideal reverberation times for speech (typically 0.5-0.7 s) (YANG, BRADLEY, 2009), the SNR component is more important for obtaining close to optimum conditions. Similarly decreasing reverberant sound would also decrease speech intelligibility because at some point decreasing reverberation leads to decreased early-arriving sound.



Fig. 2. Calculated STI values versus mean frequencyweighted  $U_{50}$  values from 125 Hz to 4000 Hz for the 12 occupied classrooms.

When the mean STI values are plotted versus the mean frequency-weighted  $U_{50}$  (STI, 125–4000) values

for the 12 occupied classrooms in Fig. 2, they show a very good fit to the linear regression line with a very small amount of scatter ( $R^2 = 0.968$  and the standard deviation about the regression line of  $\sigma = 0.007$ ). The present results agree well with the results reported in previous studies (BRADLEY *et al.*, 1999; NIJS, RYCHTÁRIKOVÁ, 2011). Figure 2 shows a 0.114 increase of STI values per 1 dB increase of  $U_{50}$  values. The results in Fig. 2 show that classrooms with  $U_{50}$ values greater than +0.5 dB will have STI values of about 0.60 or higher, which indicates 'good' acoustical conditions for speech intelligibility. That is, both measures provide approximately the same information and one can use the linear regression in Fig. 2 to convert values of one measure to values of the other measure.

A  $U_{50}$  value of +0.5 dB is 1.5 dB and 1 dB lower than the values in two previous studies by BRADLEY and BISTAFA (2002) and NIJS and RYCHTÁRIKOVÁ (2011), respectively. This is mainly because there is no standard procedure for including how to combine information at different frequencies and weightings to obtain  $U_{50}$  values. In the present study, the frequencyweighted  $U_{50}$  values averaged from 125 to 4000 Hz were used, while NJIS and RYCHTÁRIKOVÁ used the frequency-averaged  $U_{50}$  values from 63 to 4000 Hz and BRADLEY and BISTAFA used a 1 kHz  $U_{50}$  value for predicting speech intelligibility. It is not well established how to combine information at different frequencies for  $U_{50}$  best and what is the most optimal way to combine room acoustics and SNR components.

# 3.3. Practical application to the classroom acoustical design

The design of classrooms for achieving high speech intelligibility is definitely an optimisation problem. One must understand that the optimisation process is to minimise ambient noise levels to achieve acceptable speech-to-noise ratios. The SNR component is the most critical for obtaining close to optimum conditions for speech communication. One should realise that achieving an optimum reverberation time is of secondary importance because the optimum reverberation time varies when speech and noise levels are changed (YANG, BRADLEY, 2009). Either too short or too long reverberation time will decrease speech intelligibility.

The speech and noise levels measured in active classrooms (HODGSON *et al.*, 1999; SATO, BRADLEY, 2008) were quite different from values measured in quietly occupied classrooms. In most cases, the ideal goal of a +15 dB S/N ratio seems to be rarely achieved in active classrooms (HODGSON *et al.*, 1999; SATO, BRADLEY, 2008). There is a clear need for more representative data and complete understanding of speech and noise levels in occupied classrooms with teaching activities. Although both measures, STI and  $U_{50}$ , appear to be very different in a basic concept, the two measures are highly correlated and essentially assess the same characteristics of the rooms (BRADLEY *et al.*, 1999; NIJS, RYCHTÁRIKOVÁ, 2012). It is difficult to measure the STI values using amplitude-modulated noise during active speech communication in classrooms. On the other hand,  $U_{50}$  values can be easily obtained from both signal-to-noise ratios and  $C_{50}$  values in classrooms during speech communication. It is more difficult to measure these parameters in occupied classrooms and hence being able to predict values of these acoustical parameters for real speech communication is a great asset for achieving acoustically successful classrooms. The  $U_{50}$  measure can be more practically useful means of assessing and understanding room acoustics conditions for real speech communication.

## 4. Conclusions

The results illustrate that useful-to-detrimental sound ratios  $(U_{50})$  can be used to measure the combined effects of room acoustics  $(C_{50})$  and SNR values on speech intelligibility in classrooms essentially as accurately as STI values. However, all details of a standard procedure for combining information at different frequencies to obtain  $U_{50}$  should be determined and evaluated from a wide range of conditions in real classrooms. Further investigations could include the investigation of relationships between  $U_{50}$  values and speech intelligibility scores. Because the  $U_{50}$  measure is based on the same basic idea as other room acoustics parameters, such as  $C_{50}$  values, it can be a more practically useful means of assessing and understanding room acoustics conditions for speech.

The mean STI and frequency-weighted  $U_{50}$  (STI, 125–4000 Hz) values for the 12 occupied classrooms were shown to be highly correlated with  $U_{50}$  values and essentially describe the same properties of the rooms. The present results show that for classrooms with  $U_{50}$  values greater than 0.5 dB STI values are about 0.60, which indicates 'good' acoustical conditions for speech intelligibility.

#### Acknowledgments

I am very grateful to undergraduate students in the architectural engineering course at Kangwon National University who volunteered to be occupants for the classroom measurements. This work was supported by the National Research Foundation of Korea Grant funded by the Korean Government (2015R1D1A1A01056575).

#### References

1. ANSI S12.60 (2004), Acoustics performance criteria, design requirements, and guidelines for schools, American National Standards Institute, New York.

- ANSI S3.5 (1997), American National Standard Methods for Calculation of the Speech Intelligibility Index, American National Standards Institute New York.
- BRADLEY J.S. (1986), Speech intelligibility studies in classrooms, Journal of the Acoustical Society of America, 80, 846–854.
- 4. BRADLEY J.S. (2011), Using room acoustics measures to understand a large room and sound reinforcement system, Proceedings of the Institute of Acoustics, 33.
- BRADLEY J.S., BISTAFA S.R. (2002), Relating speech intelligibility to useful-to-detrimental sound ratios, Journal of the Acoustical Society of America, 112, 27– 29.
- BRADLEY J.S., REICH R., NORCROSS S.G. (1999), On the combined effects of signal-to-noise ratio and room acoustics on speech intelligibility, Journal of the Acoustical Society of America, 106, 1820–1828.
- CHOI Y.J. (2016), Effect of occupancy on acoustical conditions in university classrooms, Applied Acoustics, 114, 36–43.
- DIRAC room acoustics software version 6.0 (2014), Brüel & Kjær, Denmark.
- HODGSON M. (2002), Rating, ranking, understanding acoustical quality in university classrooms, Journal of the Acoustical Society of America, 112, 568–575.
- HODGSON M., NOSAL E.-M. (2002), Effect of noise and occupancy on optimal reverberation times for speech intelligibility in classrooms, Journal of the Acoustical Society of America, 111, 931–939.
- HODGSON M., REMPEL R., KENNEDY S. (1999), Measurement and prediction of typical speech and background noise level in university classrooms during lectures, Journal of the Acoustical Society of America, 105, 226–233.
- 12. IEC 60268-16 Edition 4.0 (2011), Sound system equipment. Part 16: Objective rating of speech intelligibility by speech transmission index.
- 13. ISO 3382 (2003), Acoustics. Measurement of the reverberation time of rooms with reference to other acoustical parameters.
- NIJS L., RYCHTÁRIKOVÁ M. (2011), Calculating the optimum reverberation time and absorption coefficient for good speech intelligibility in classroom design using U<sub>50</sub>, Acta Acustica United with Acustica, 97, 93–102.
- SATO H., BRADLEY J.S. (2008), Evaluation of acoustical conditions for speech communication in working elementary school classrooms, Journal of the Acoustical Society of America, 123, 2064–2077.
- SCHROEDER M.R. (1981), Modulation transfer functions: Definition and Measurement, Acustica, 49, 179– 182.
- YANG W.S., BRADLEY J.S. (2009), Effects of room acoustics on the intelligibility of speech in classrooms for young children, Journal of the Acoustical Society of America, 125, 922–933.